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APPLICATION OF

WILLIAM SCOTT WALSTON, JON C. SCHAEFFER, AND
WENDY HOWARD MURPHY

for

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on

LOW-SULFUR ARTICLE HAVING A PLATINUM-ALUMINIDE
PROTECTIVE LAYER, AND ITS PREPARATION

LOW-SULFUR ARTICLE HAVING A PLATINUM-ALUMINIDE PROTECTIVE LAYER, AND ITS PREPARATION

This application is a continuation-in-part of application Ser. No. 09/149,018, filed September 8, 1998, for which priority is claimed and whose disclosure is incorporated by reference.

BACKGROUND OF THE INVENTION

This application relates to coated articles, and, more particularly, to a superalloy article having a metallic overlay protective coating.

In an aircraft gas turbine (jet) engine, air is drawn into the front of the engine, compressed by a shaft-mounted compressor, and mixed with fuel. The mixture is burned, and the hot exhaust gases are passed through a turbine mounted on the same shaft. The flow of combustion gas turns the turbine, which turns the shaft and provides power to the compressor. The hot exhaust gases flow from the back of the engine, driving it and the aircraft forwardly.

The hotter the combustion and exhaust gases, the more efficient is the operation of the jet engine. There is thus an incentive to raise the combustion and exhaust gas temperatures. However, the maximum temperature of the combustion gases is normally limited by the materials used to fabricate the turbine vanes and turbine blades of the turbine. In current engines, the turbine vanes and blades are made of nickel-based superalloys, and can operate at temperatures of up to 1900-2100F.

Many approaches have been used to increase the operating temperature limit of the turbine blades and vanes to their current levels. The composition and processing of the materials themselves have been improved, and physical cooling techniques are employed.

In another approach, a protective layer or a ceramic/metal thermal barrier coating (TBC) system is applied to the turbine blade or turbine vane component,

which acts as a substrate. The protective layer with no overlying ceramic layer (in which case the protective layer is termed an "environmental coating") is useful in intermediate-temperature applications. The currently known protective layers include diffusion aluminides and MCrAlY(X) overlays.

A ceramic thermal barrier coating layer may be applied overlying the protective layer, to form a thermal barrier coating system (in which case the protective layer is termed a "bond coat"). The thermal barrier coating system is useful in higher-temperature applications. The ceramic thermal barrier coating insulates the component from the combustion gas, permitting the combustion gas to be hotter than would otherwise be possible with the particular material and fabrication process of the substrate.

Although these coating systems are operable, there is always the need to achieve further improvements in maximum operating temperatures and times of coated articles. The present invention fulfills this need, and further provides related advantages.

BRIEF SUMMARY OF THE INVENTION

The present invention provides a method for preparing a coated article protected by a protective layer, and the article itself. The protective layer is suitable for use as an environmental coating with no overlying thermal barrier coating, or as the bond coat for a thermal barrier coating. The elevated temperature oxidation performance of the coated article is improved over that of conventional coated articles.

A coated article comprises an article substrate having a free sulfur content of more than 0 but less than about 1 part per million by weight (ppmw), and a protective layer at a surface of the article substrate. The article substrate is preferably a nickel-base superalloy, in the shape of a component of a gas turbine aircraft engine such as a turbine blade or turbine vane. The protective layer comprises a platinum aluminide diffusion coating. A thermal barrier coating layer made of a ceramic such as yttria-stabilized zirconia may overlie the protective

layer, which is then termed a bond coat. There may instead be no overlying ceramic thermal barrier coating layer, in which case the protective layer is termed an environmental coating. Both the protective layer and the ceramic thermal barrier coating layer, where present, are also low in sulfur, preferably less than about 1 ppm by weight.

The protective layer may be substantially yttrium free, with less than about 10 parts per million. The protective layer may instead contain a substantial amount of yttrium, typically from about 10 to about 200 parts per million, for other applications.

The substrate article with low free sulfur content may be furnished in a variety of ways. The base metal may be selected to have a low free sulfur content. The composition of the base metal may be modified to result in a low free sulfur content. In one approach, a sulfur-scavenging element such as hafnium or zirconium is provided in the base metal in an amount sufficient to reduce the free sulfur content to less than about 1 part per million (ppm) by weight. In another approach, a conventional high-sulfur base metal can be provided. The base metal is contacted to a reducing gas to remove sulfur and reduce the free sulfur to the required low level. For example, the base metal can be contacted at elevated temperatures to hydrogen or a hydrogen-containing gas that desulfurizes the metal. In yet another approach, the molten base metal may be placed into contact with a reactive element such as calcium or magnesium, to react with and reduce the free sulfur content.

In the past, in many instances the sulfur content of the underlying substrate upon which the protective layer is deposited has not been reported. It may not be concluded from the absence of reporting of the sulfur content that the sulfur content is zero or otherwise less than about 1 part per million. Instead, in such situations it may be concluded that the sulfur content is likely in the typical range of about 5 to about 30 parts per million by weight, and that the sulfur content was not reported because there was no realization of its significance at the time.

The coated article of this type can be used in high-temperature applications in severe environments. A preferred application is as a gas turbine blade or vane,

but the invention is not so limited. Other features and advantages of the present invention will be apparent from the following more detailed description of the preferred embodiment, taken in conjunction with the accompanying drawings, which illustrate, by way of example, the principles of the invention.

BRIEF DESCRIPTION OF THE DRAWINGS

Figure 1 is a perspective view of a gas turbine component article;

Figure 2 is a sectional view through the article of Figure 1, taken generally along line 2-2, illustrating a protective layer on the surface of the article; and

Figure 3 is a block diagram of one embodiment of the approach of the invention.

DETAILED DESCRIPTION OF THE INVENTION

Figure 1 depicts a component of an aircraft gas turbine engine such as a turbine blade or turbine vane, and in this case is depicted as a turbine blade 20. Other gas turbine engine components can benefit from the coating approach of the invention, such as, for example, combustor liners, turbine seals, exhaust nozzles, and shrouds. The turbine blade 20 includes an airfoil 22 against which the flow of hot exhaust gas is directed. The turbine blade 20 is mounted to a turbine disk (not shown) by a dovetail 24 which extends downwardly from the airfoil 22 and engages a slot on the turbine disk. A platform 26 extends longitudinally outwardly from the area where the airfoil 22 is joined to the dovetail 24. A number of cooling channels may extend through the interior of the airfoil 22, ending in openings 28 in the surface of the airfoil 22. A flow of cooling air is directed through the cooling channels, to reduce the temperature of the airfoil 22.

Figure 2 illustrates a protective system 30 deposited upon the turbine blade 20, which thereby acts as a substrate 32. The substrate 32 may be formed of any operable material, but a preferred base metal from which the article substrate is formed is a nickel-base superalloy. A nickel-base superalloy has more nickel than

any other element. A preferred nickel-base alloy is Rene N5, which has a nominal composition in weight percent of 7.5 percent cobalt, 7 percent chromium, 6.2 percent aluminum, 6.5 percent tantalum, 5 percent tungsten, 1.5 percent molybdenum, 3 percent rhenium, balance nickel. The article substrate is

preferably, but not necessarily, directionally solidified or single crystal.

The substrate 32 has a free sulfur content of less than about 1 part per million by weight (ppmw), more preferably less than about 0.5 parts per million by weight, and most preferably on the order of about 0.2 parts per million by weight. Larger amounts of free sulfur interfere with the adherence of coatings to the surface of the substrate during service. The free sulfur content need meet this requirement only locally, near the surface of the substrate 32. Because sulfur diffuses through the substrate 32 during elevated temperature exposure, it is, however, preferred that the free sulfur content be below about 1 ppm throughout at least most of, and most preferably all, the substrate material.

The substrate 32 has a yttrium content of no greater than about 200 parts per million by weight. If the substrate has a yttrium content of more than about 200 parts per million by weight, it is extremely difficult to cast, with the result that manufacturing costs are increased, and the added yttrium increases the cost but has little added effect on improved properties. For less demanding applications, the substrate has substantially no yttrium, which is herein defined as less than about 10 parts per million by weight yttrium. The yttrium in this range adds little to the cost of the substrate material, and does not substantially increase the difficulty in casting the substrate material. However, in some more demanding applications such as articles exposed to very high temperatures for extended periods of time, the yttrium is present in an amount of from about 10 to about 200 parts per million by weight. The added cost and casting difficulties associated with this higher yttrium range are offset by the improved performance that is achieved with more than about 10 parts per million by weight of yttrium.

A protective layer 34 is present at a free surface 36 of the substrate 32. The protective layer 34 is a diffusion platinum aluminide. The diffusion platinum aluminide of the protective layer 34 of Figure 2 is a metallic composition

containing platinum, aluminum, and the elements present in the substrate 32. The diffusion aluminide is formed by depositing one or more sublayers overlying the surface 36, and then interdiffusing the deposited sublayers. For example, a sublayer containing platinum is first deposited upon the free surface 36, and then a sublayer containing aluminum is deposited over the platinum sublayer at a

temperature sufficient that the platinum and aluminum sublayers interdiffuse with each other and with the material of the substrate to form a platinum-aluminum coating layer. In a preferred embodiment, the platinum is present in an average amount of from about 20 to about 30 weight percent, preferably from about 25 to about 28 weight percent, of the protective layer 34, and the aluminum is present in an average amount of from about 14 to about 25 weight percent, preferably from about 18 to about 22 weight percent, of the protective layer 34. The remainder of the protective layer 34 comprises elements interdiffused from the substrate 32. The protective layer 34 is preferably from about 0.0005 to about 0.004 inches in thickness, but lesser or greater thicknesses are operable although less desirable.

A ceramic layer 38 optionally overlies the protective layer 34. The ceramic layer 34 is preferably yttria-stabilized zirconia, which is zirconium oxide containing from about 6 to about 8 weight percent of yttrium oxide. Other operable ceramic materials may be used as well. The ceramic layer 34 is preferably from about 0.004 inch to about 0.025 inch thick, most preferably from about 0.005 inch to about 0.015 inch thick. (Figure 2 is not drawn to scale.)

Figure 3 depicts a method of preparing a coated article such as the turbine blade 20. An article substrate 32 having a free sulfur content of less than about 1 part per million by weight, preferably less than 0.5 parts per million by weight, and most preferably about 0.2 parts per million by weight, is furnished, numeral 50. The article substrate preferably comprises a nickel-base superalloy such as Rene' N5 alloy, whose composition is set forth above, with the above-discussed sulfur limitation. The article substrate 32 has the shape of the final desired coated article, with the same dimensions reduced only by an allowance for the thickness, if any, of the protective system. In the case depicted in Figure 1, the article substrate 32 would have the shape of the turbine blade 20. In a typical

commercial operation, the base metal of the article substrate 32 is melted and then cast into the shape of the article substrate by directional solidification to produce an oriented microstructure in the article substrate.

As used herein, "free sulfur" is sulfur present in elemental form and not chemically combined with another element. Free sulfur is to be contrasted with

combined sulfur, in which the sulfur is chemically combined with one or more other elements. The total sulfur content is the free sulfur content plus the combined sulfur content. The important distinction between free sulfur and combined sulfur, for the present purposes, is that free sulfur can diffuse to the surface 36 of the substrate 32 and promote the debonding of the protective system 30 from the substrate 32. Combined sulfur, on the other hand, is fixed at a single location and cannot move to the surface of the article substrate.

The article substrate 32 having a free sulfur content of below about 1 part per million by weight can be achieved in several ways. In one, only those heats of material having such a sulfur content would be selected and used to fabricate the article substrate. This approach is expected to have limited usefulness, because most alloys tend to have larger amounts of sulfur present due to their method of melting and casting.

In another and currently preferred approach, a scavenger element that reacts with free sulfur to produce combined sulfur may be present in the molten base metal which is used to make the article substrate. The scavenger element must be present in a sufficient amount to reduce the remaining free sulfur--that sulfur which does not react to produce combined sulfur--to the required low level of less than about 1 part per million by weight. The scavenger element is preferably calcium, which reacts with free sulfur to produce calcium sulfide, or magnesium, which reacts with free sulfur to produce magnesium sulfide.

In another approach, the article substrate is made of a base metal having a free sulfur content of more than about 1 part per million by weight. The article substrate is thereafter processed to reduce its sulfur content to less than about 1 part per million by weight. The preferred processing is achieved by contacting the article substrate to a reducing gas at elevated temperature. The reducing gas

reduces and reacts with the sulfur at the surface of the article substrate to produce a gaseous sulfide which is carried away into the gaseous atmosphere. Any native oxide present at the surface of the substrate must not act as a barrier to sulfur removal in this process. If any such barrier is present, it must be removed prior to the sulfur-removal treatment. Sulfur that is initially within the interior of the article substrate diffuses to the surface, and is in turn reduced and reacted to

remove it from the substrate. The process is continued until the sulfur content of the article substrate is reduced to the required level. Desulfurization is achieved by heating the article substrate 32 in a reducing atmosphere, preferably 1 atmosphere of flowing hydrogen gas or other hydrogen-containing gas, to a high temperature for a period of time sufficient to react and remove the sulfur from the substrate. For nickel-base superalloys, the desulfurization heat treatment temperature is conducted at at least about 2200°F, to achieve the required degree of desulfurization in a commercially acceptable time. The temperature to which the substrate is heated will depend upon the composition of the substrate. For the preferred Rene N5 substrate, a temperature of about 2250-2340°F is preferred. For an actual substrate in the form of a turbine blade airfoil, desulfurization was successfully completed by exposure to 1 atmosphere of flowing hydrogen gas at 2336°F in a time of 100 hours.

The desulfurization treatment, when used, is preferably conducted during melting of the alloy, which is thereafter cast into the desired shape of the article substrate. Equivalently for the present purposes, the desulfurization may be performed after the casting of the base metal to form the article substrate, and just before the deposition of the protective system 30. If the metal is desulfurized prior to forming the article substrate, care must be taken so that sulfur is not re-introduced when the article substrate is formed.

The protective system 30 is formed on the free surface 36 of the substrate 32. The protective layer 34 is formed by any operable process. Preferably, a platinum sublayer is first deposited. The deposition is accomplished by electrodepositing platinum from a platinum-containing solution onto the substrate. An operable platinum-containing solution is an aqueous solution of 4-20 grams

platinum per liter of platinum provided as $\text{Pt}(\text{NH}_3)_4\text{HPO}_4$, and the voltage/current source is operated at 1/2 to 10 amperes per square foot of surface being electroplated. A platinum sublayer about 5 micrometers thick is deposited in 1-4 hours at a temperature of 190-200°F.

An aluminum sublayer is deposited overlying the platinum sublayer 34. The aluminum sublayer is deposited by any operable approach, with vapor deposition preferred. In that approach, a hydrogen halide gas, such as hydrogen

chloride, is contacted with aluminum metal or an aluminum alloy to form the corresponding aluminum halide gas. The aluminum halide gas contacts the platinum sublayer already deposited on the substrate, depositing the aluminum thereon. The deposition occurs at elevated temperature such as from about 1925°F to about 1975°F so that the deposited aluminum atoms interdiffuse into the platinum layer 34 during a 4 to 20 hour cycle. This technique allows doping or alloying elements to be deposited into the aluminum sublayer if desired, from the halide gas. During this deposition the aluminum sublayer, the platinum sublayer, and the metal of the substrate interdiffuse to form the platinum aluminide. Additional interdiffusion may be accomplished if desired by maintaining the structure at elevated temperature after the flow of halide gas is discontinued. The platinum and aluminum sublayers interdiffused with the substrate form the protective layer 34 that inhibits oxidation and corrosion damage to the airfoil 22, during exposure at intermediate temperatures.

The ceramic layer 38 is optionally applied overlying and contacting the protective layer 34, numeral 54 of Figure 3. The ceramic layer 38 may be deposited by any operable technique, with electron beam physical vapor deposition (EBPVD) being preferred. Other techniques include, for example, air plasma spray, low pressure plasma spray, and electron beam physical vapor deposition.

Although particular embodiments of the invention have been described in detail for purposes of illustration, various modifications and enhancements may be made without departing from the spirit and scope of the invention. Accordingly, the invention is not to be limited except as by the appended claims.